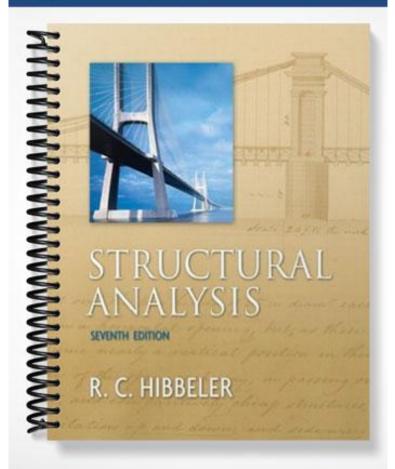
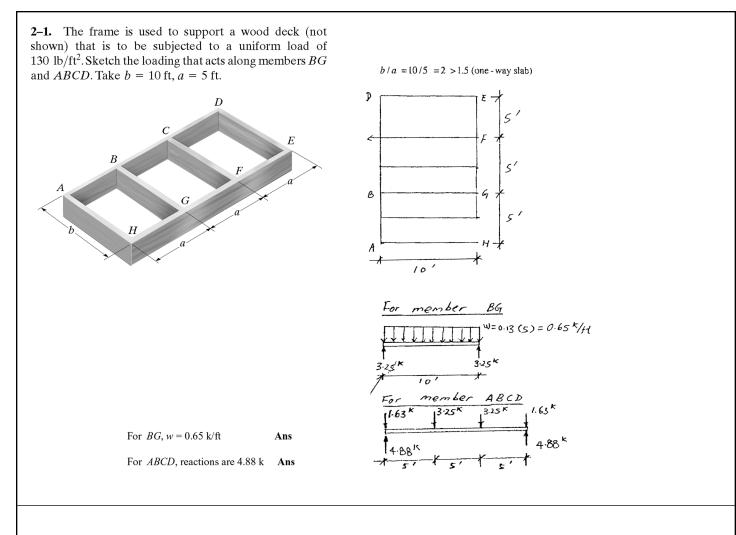
## SOLUTIONS MANUAL



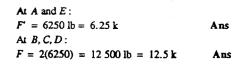


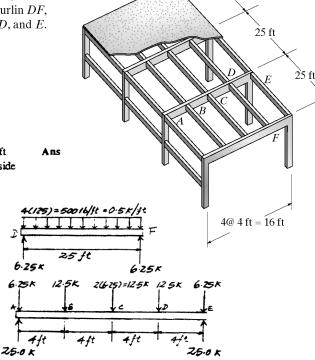
2-2. The roof deck of the single story building is subjected to a dead plus live load of 125 lb/ft<sup>2</sup>. If the purlins are spaced 4 ft and the bents are spaced 25 ft apart, determine the distributed loading that acts along the purlin DF, and the loadings that act on the bent at A, B, C, D, and E.

$$\frac{L_2}{L_1} = \frac{25}{4} = 6.25 > 2$$

## One - way slab.

Tributary load along  $DF = (125 \text{ lb/ft}^2)(4 \text{ ft}) = 500 \text{ lb/ft}$ This load is also transferred to the bent from the other side of AE. Half the tributary loading acts at A and E.

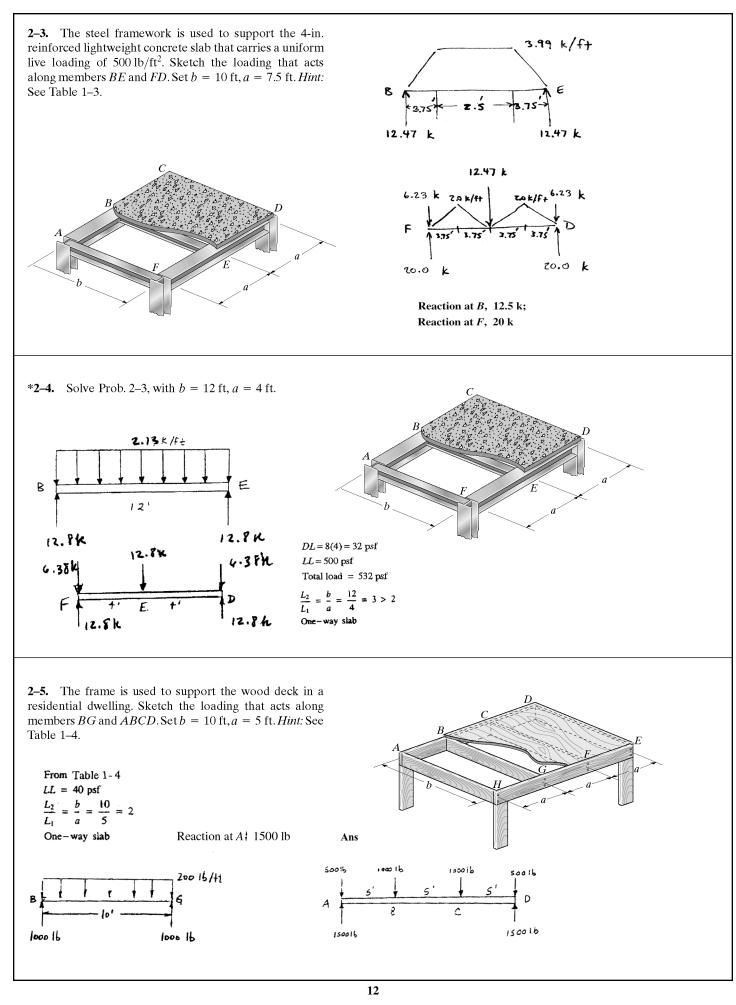


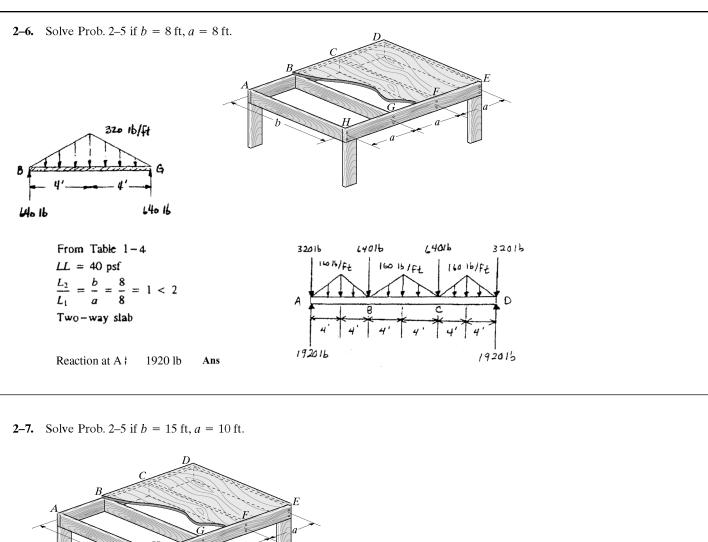


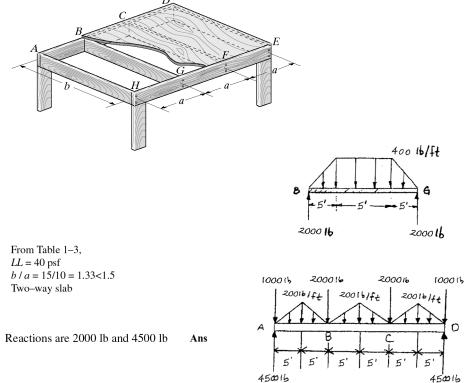
25 ft

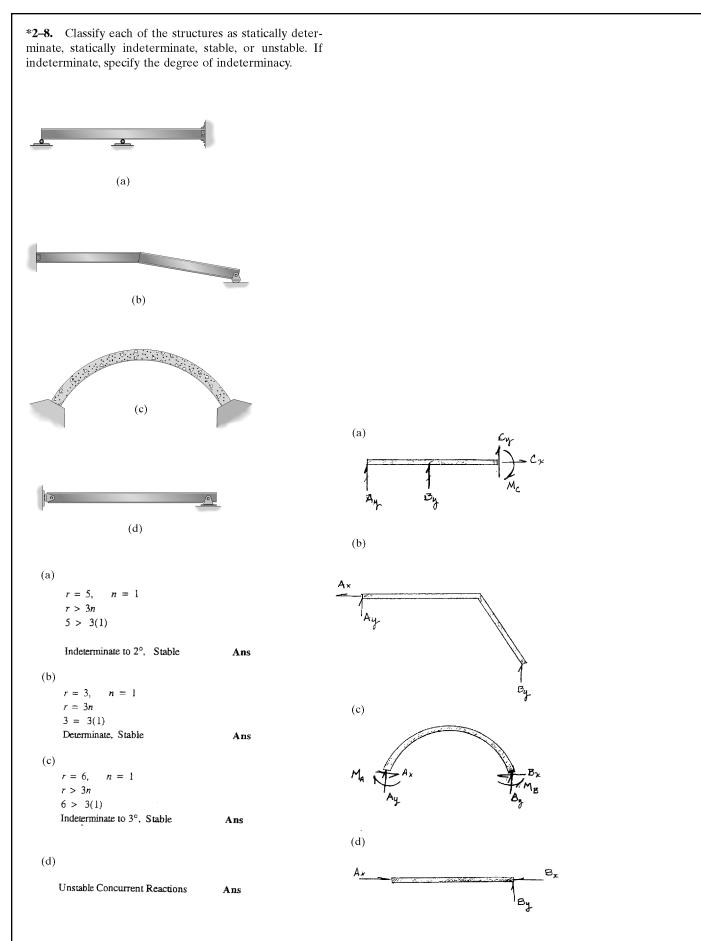
11

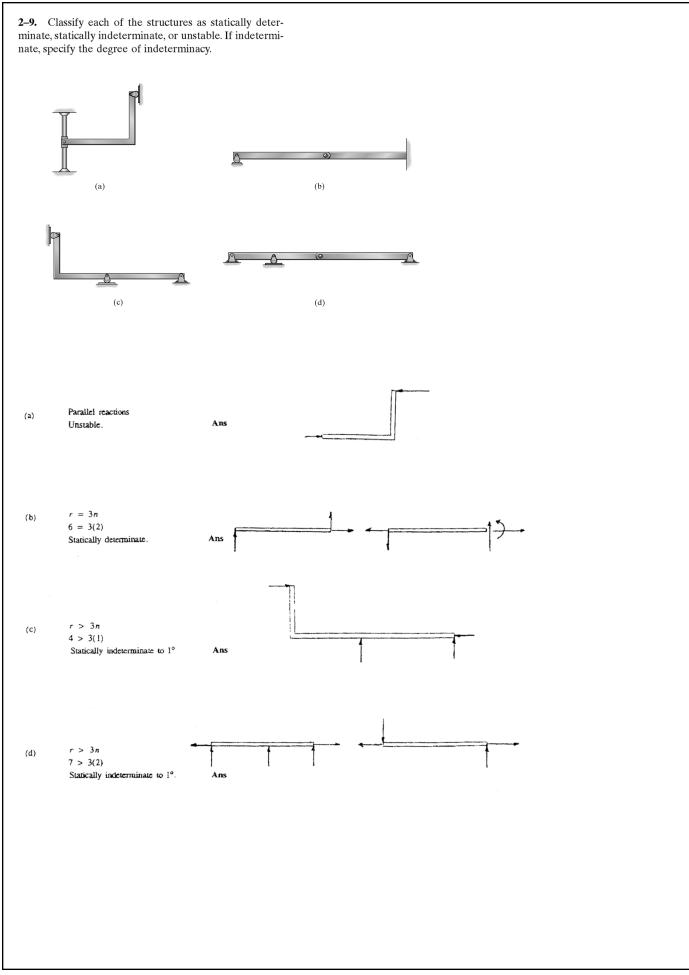
6.25K







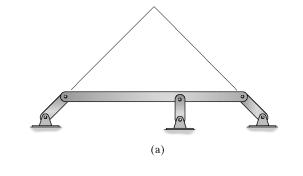




(.)

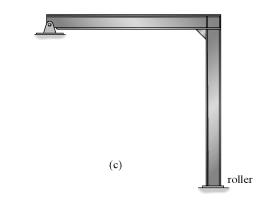
- 2

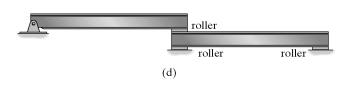
**2–10.** Classify each of the structures as statically determinate, statically indeterminate, or unstable. If indeterminate, specify the degree of indeterminacy.







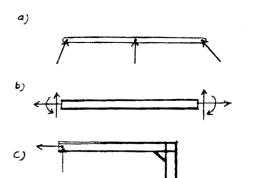




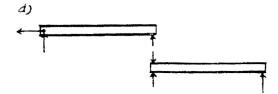
(=)	Statically determinate	Ans
<b>(</b> b)	r = 6 $3n = 3(1) = 3 < 6Indeterminate to 3°$	Ans
(c)	r = 3 $3n = 3(1) = 3Statically determinate$	Aas

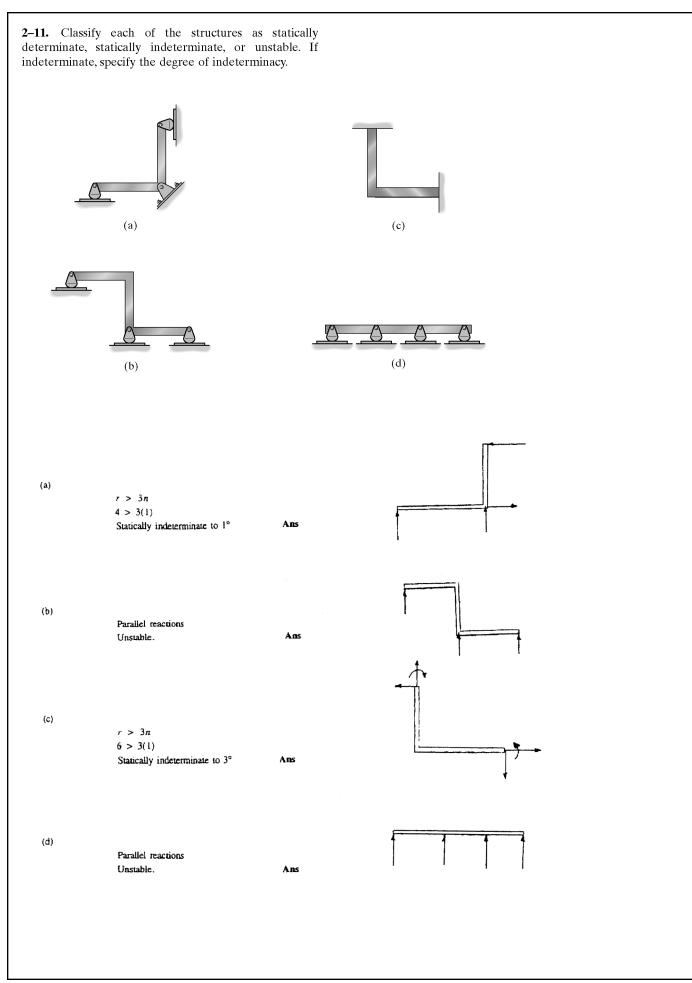
 $3_{11} = 3(1) = 3$ 

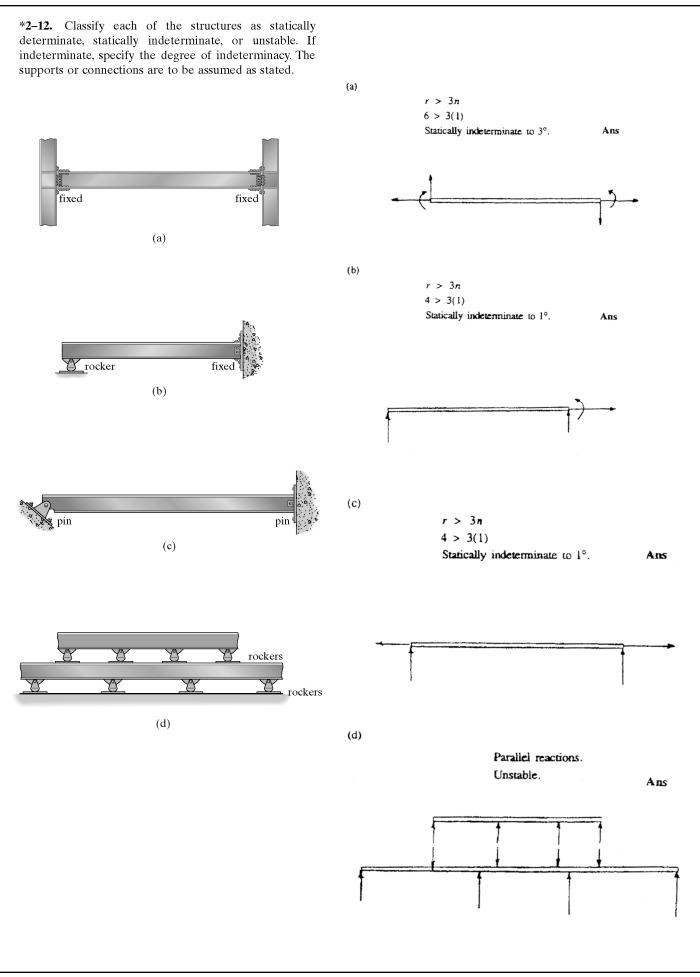
(d) Parallel reactions on lower beam Unstable Ans

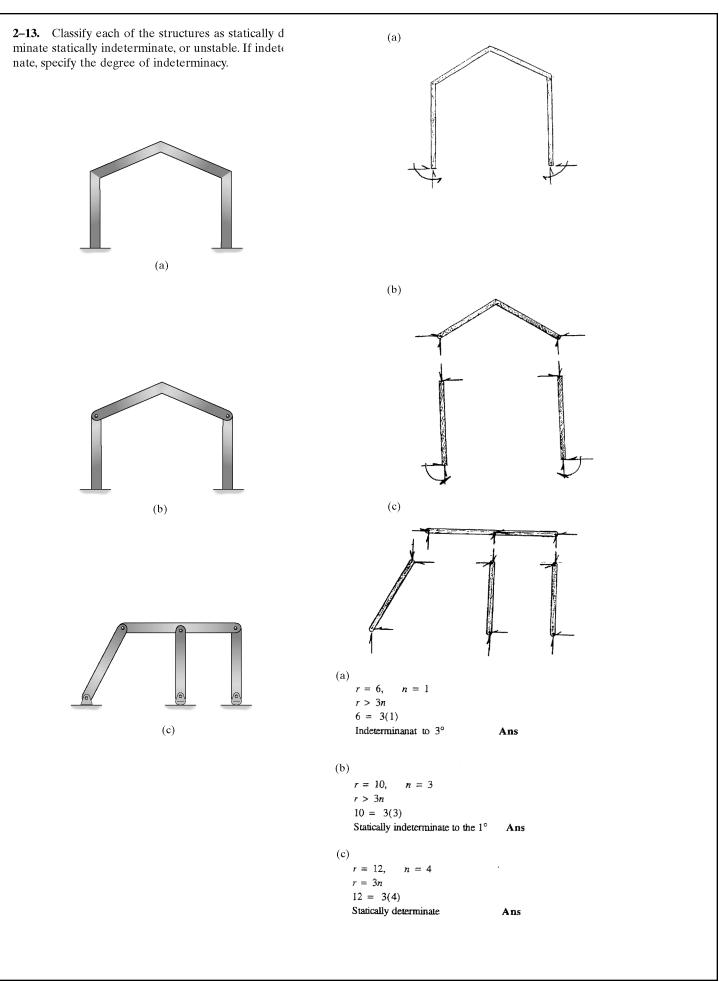


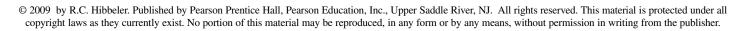


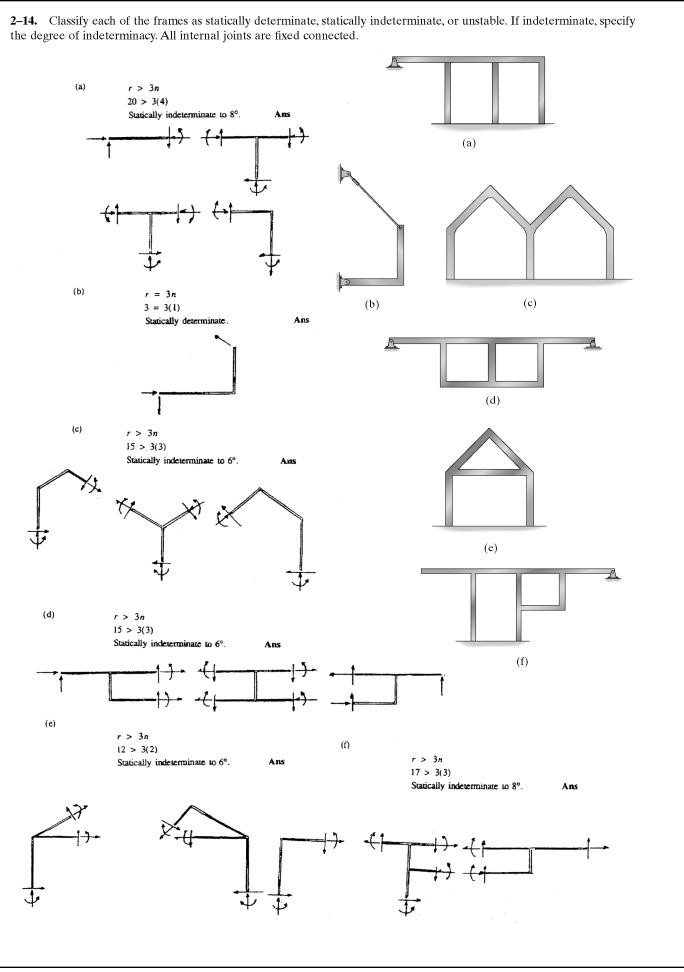






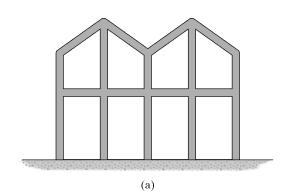


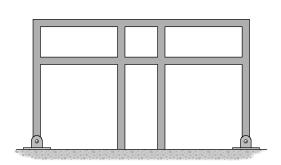




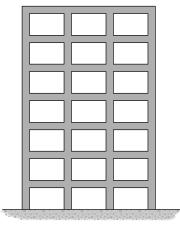
(a)

**2–15.** Determine the degree to which the frames are statically indeterminate. All internal joints are fixed connected.





(b)



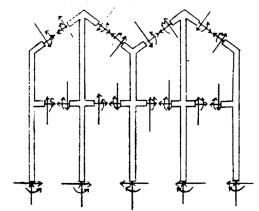
(c)

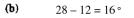
(b) Statically indeterminate to 16° Ans Statically indeterminate to 63° Ans

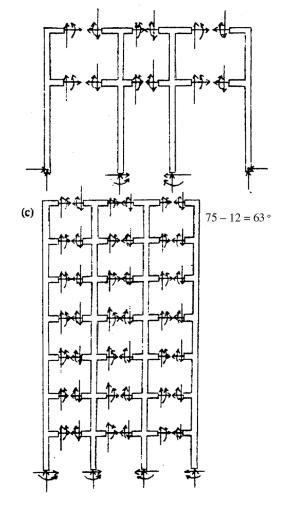
Ans

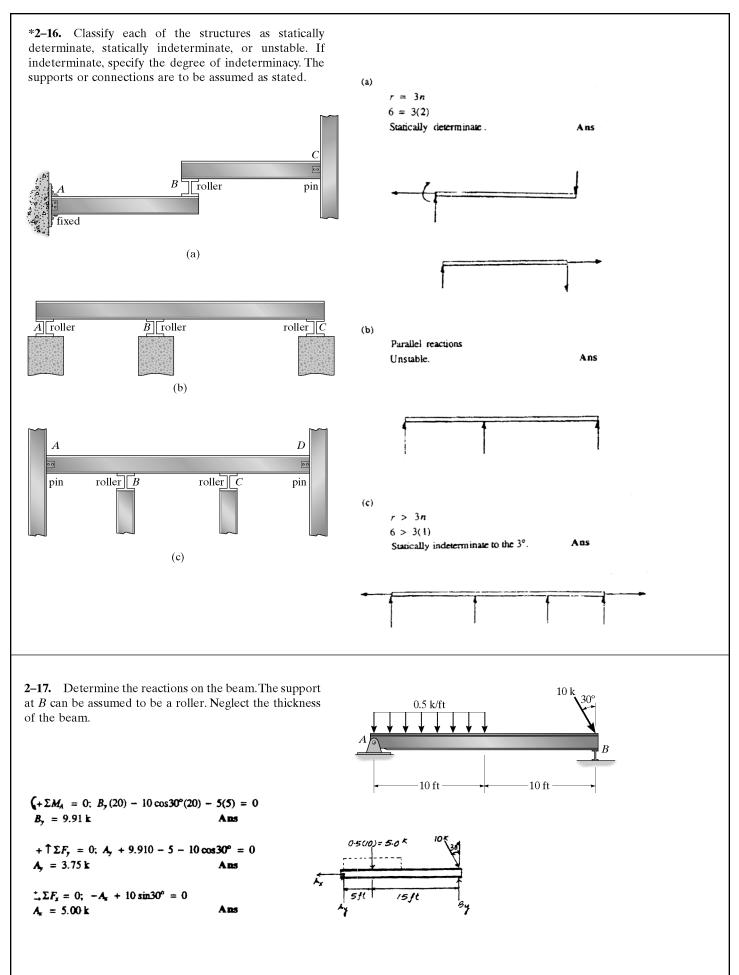
Statically indeterminate to 24°

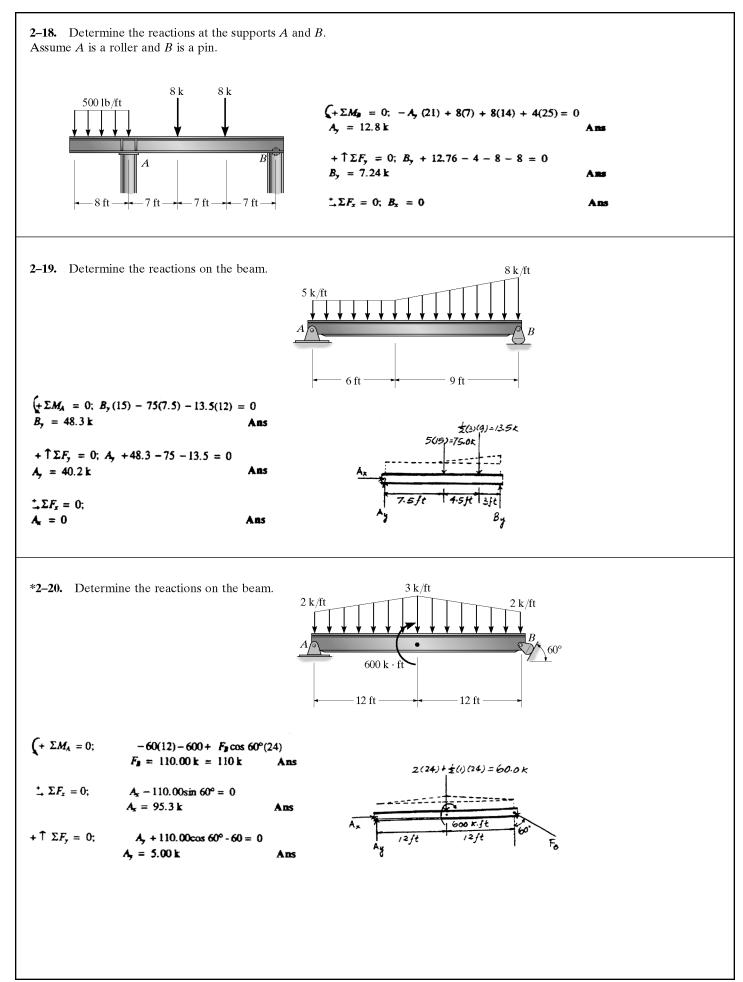
(a)  $39 - 15 = 24^{\circ}$ 

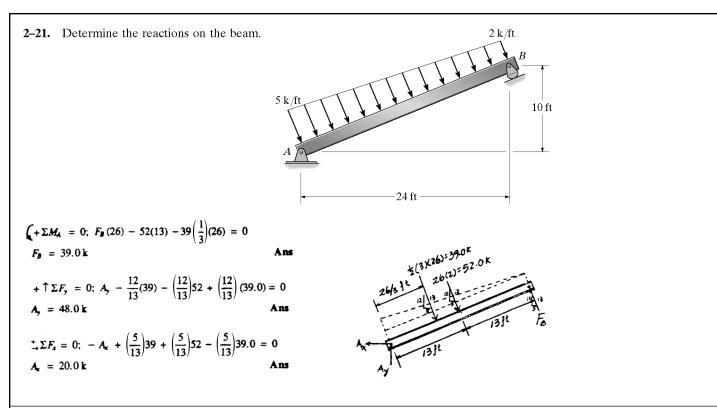




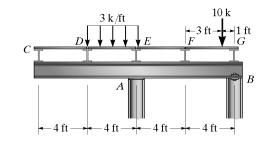


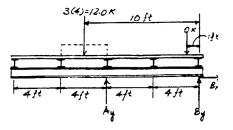






**2-22.** Determine the reactions at the supports A and B. The floor decks CD, DE, EF, and FG transmit their loads to the girder on smooth supports. Assume A is a roller and B is a pin.



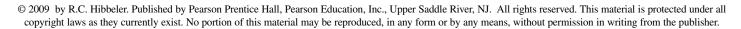


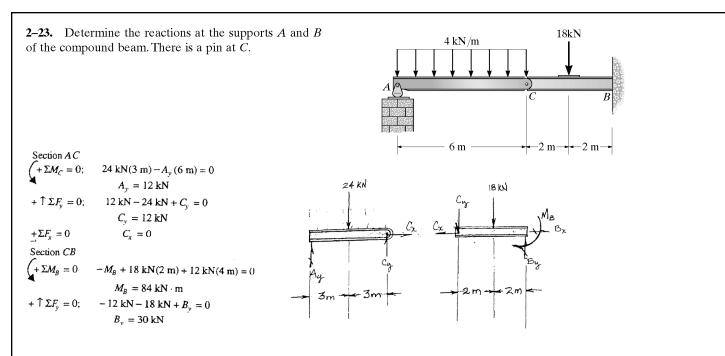
Consider the entire system.

$$\begin{cases} +\Sigma M_B = 0; \ 10(1) + 12(10) - A_y(8) = 0 \\ A_y = 16.25 \, k = 16.3 \, k \end{cases}$$
 Ans

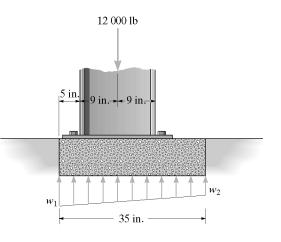
$$L_{x}\Sigma F_{x} = 0; B_{x} = 0$$
 Ans

 $+\uparrow \Sigma F_y = 0; \ 16.25 - 12 - 10 + B_y = 0$  $B_y = 5.75 \text{ k}$  Ans





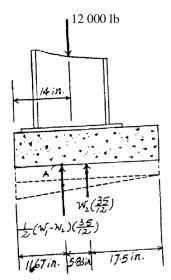
\*2-24. The pad footing is used to support the load of 12 000 lb. Determine the intensities  $w_1$  and  $w_2$  of the distributed loading acting on the base of the footing for equilibrium.

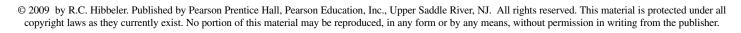


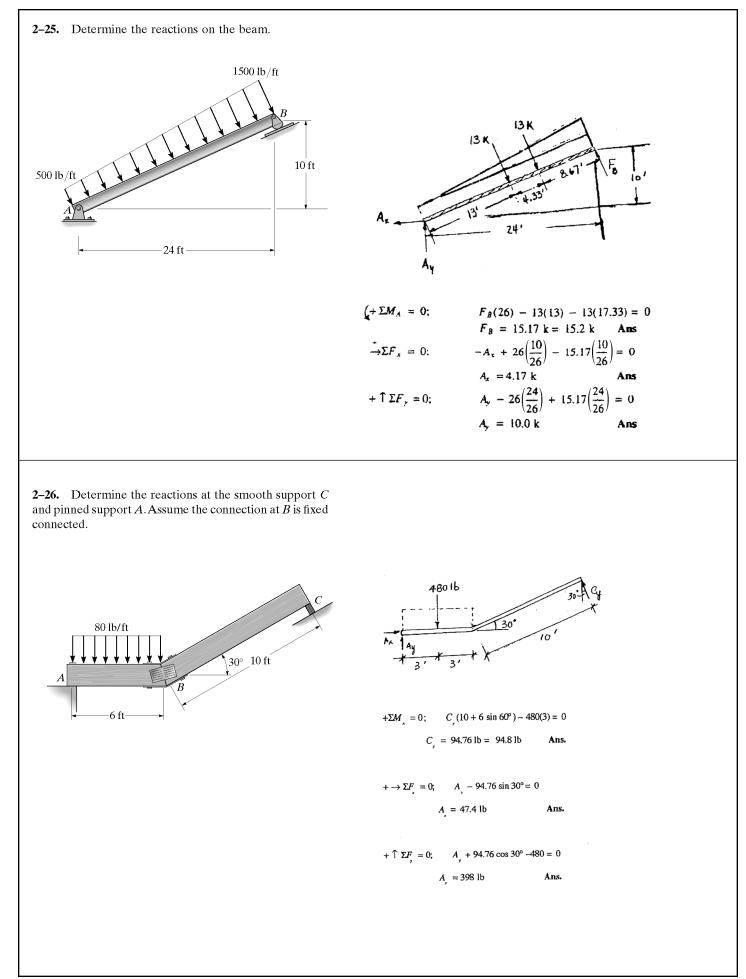
Equations of Equilibrium : The load intensity  $w_2$  can be determined directly by summing moments about point A.

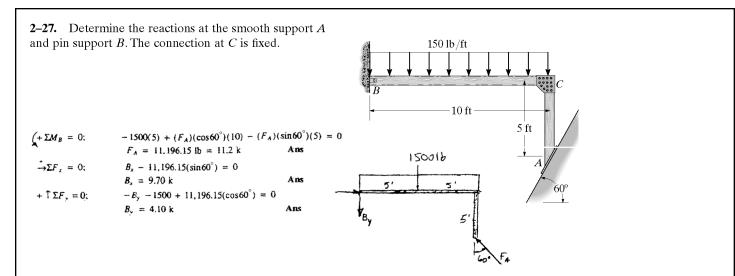
$$(+\Sigma M_A = 0; w_2 (\frac{35}{12})(17.5 - 11.67) - 12(14 - 11.67) = 0$$
  
 $w_2 = 1.646 \text{ kip/ft} = 1.65 \text{ kip/ft}$  Ans

+ 
$$\uparrow \Sigma F_y = 0;$$
  $\frac{1}{2}(w_1 - 1.646) \left(\frac{35}{12}\right) + 1.646 \left(\frac{35}{12}\right) - 12 = 0$   
 $w_1 = 6.58 \text{ kip/ft}$  Ans

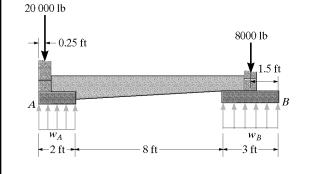


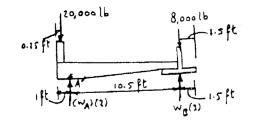






\*2-28. The cantilever footing is used to support a wall near its edge A so that it causes a uniform soil pressure under the footing. Determine the uniform distribution loads,  $w_A$  and  $w_B$ , measured in lb/ft at pads A and B, necessary to support the wall forces of 8000 lb and 20 000 lb.





 $(+\Sigma M_{A^{+}} = 0; -8000 (10.5) + w_{B} (3) (10.5) + 20 000 (0.75) = 0$ 

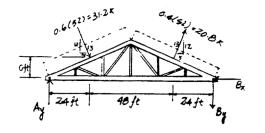
 $w_B = 2190.5 \text{ lb/ft} = 2.19 \text{ kip/ft}$  Ans

$$+\uparrow\Sigma F_{y} = 0;$$
 2190.5 (3) - 28 000 +  $w_{A}$  (2) = 0

Ans

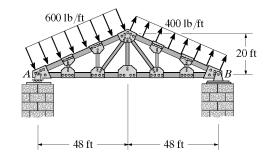
$$= 10.7 \text{ kip/ft}$$

**2–29.** Determine the reactions at the truss supports *A* and *B*. The distributed loading is caused by wind.



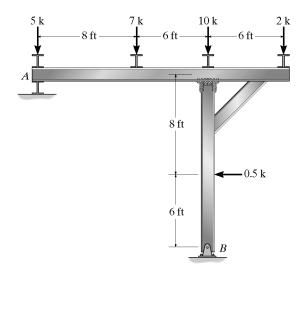
 $\begin{pmatrix} +\Sigma M_{A} = 0; -B_{y}(96) + \left(\frac{12}{13}\right)20.8(72) - \left(\frac{5}{13}\right)20.8(10) - \left(\frac{12}{13}\right)31.2(24) - \left(\frac{5}{13}\right)31.2(10) = 0 \\ B_{y} = 5.117 \text{ kN} = 5.12 \text{ kN} & \text{Ans} \\ + \uparrow \Sigma F_{y} = 0; \ A_{y} - 5.117 + \left(\frac{12}{13}\right)20.8 - \left(\frac{12}{13}\right)31.2 = 0 \\ A_{y} = 14.7 \text{ kN} & \text{Ans} \end{cases}$ 

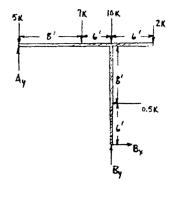
$$\therefore \Sigma F_x = 0; -B_x + \left(\frac{5}{13}\right) 31.2 + \left(\frac{5}{13}\right) 20.8 = 0$$
  
 $B_x = 20.0 \text{ kN}$  Ans



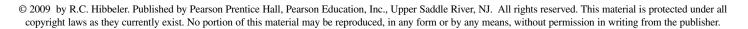
**2–30.** The jib crane is pin-connected at *A* and supported by a smooth collar at B. Determine the roller placement x of the 5000-lb load so that it gives the maximum and minimum reactions at the supports. Calculate these reactions in each case. Neglect the weight of the crane. Require 4 ft  $\leq x \leq 10$  ft. 12 ft Equations of Equilibrium :  $(+ \Sigma M_A = 0; N_B (12) - 5x = 0 N_B = 0.4167x$ [1] +  $\uparrow \Sigma F_y = 0;$   $A_y - 5 = 0$   $A_y = 5.00$  kip [2]  $\stackrel{+}{\to} \Sigma F_x = 0; \quad A_x - 0.4167x = 0 \quad A_x = 0.4167x$ [3] By observation, the maximum support reactions occur when x = 10 ftAns With x = 10 ft, from Eqs. [1], [2] and [3], the maximum support ΝB reactions are  $A_x = N_B = 4.17 \text{ kip}$   $A_y = 5.00 \text{ kip}$ Ans By observation, the minimum support reactions occur when 12ft x = 4 ft5 kip Ans With x = 4 ft, from Eqs. [1], [2] and [3], the minimum support reactions are Ar  $A_x = N_B = 1.67 \text{ kip}$   $A_y = 5.00 \text{ kip}$ Ans

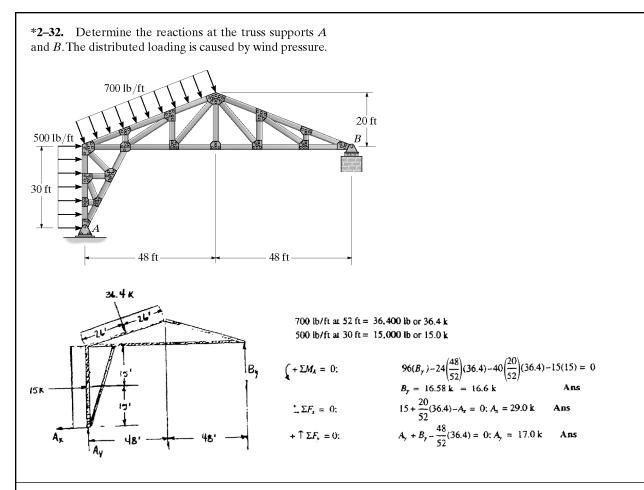
**2-31.** Determine the reactions at the supports *A* and *B* of the frame. Assume that the support at *A* is a roller.



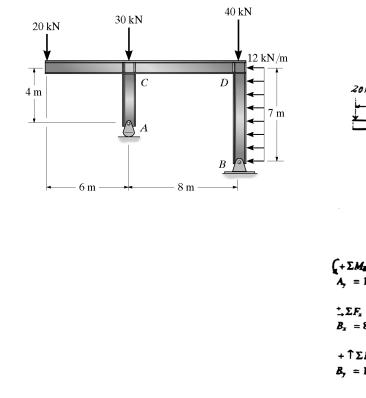


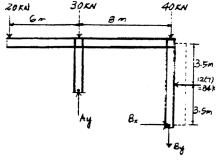
 $(+\Sigma M_B = 0; -(0.5)(6) + (2)(6) - (7)(6) - (5)(14) + A_y (14) = 0$  $A_y = 7.36 k Ans$  $+ ^ \Subset \Sigma F_y = 0; 7.36 - 5 - 7 - 10 - 2 + B_y = 0$  $B_y = 16.6 k Ans$  $- 0.5 + B_z = 0$  $B_z = 0.500 k Ans$ 





**2–33.** Determine the horizontal and vertical components of reaction at the supports A and B. The joints at C and D are fixed connections.



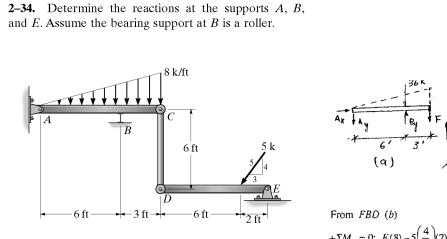


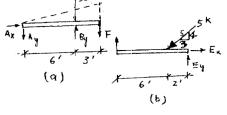
 $(+\Sigma M_{B} = 0; 20(14) + 30(8) + 84(3.5) - A_{2}(8) = 0$ A<sub>2</sub> = 101.75 kN = 102 kN

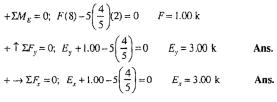
Ans

$$\Delta \Sigma F_x = 0; B_x - 84 = 0$$
  
 $B_x = 84.0 \text{ kN}$  A1  
 $+ \uparrow \Sigma F_y = 0; 101.75 - 20 - 30 - 40 - B_y = 0$ 

B, = 11.75 kN Ans

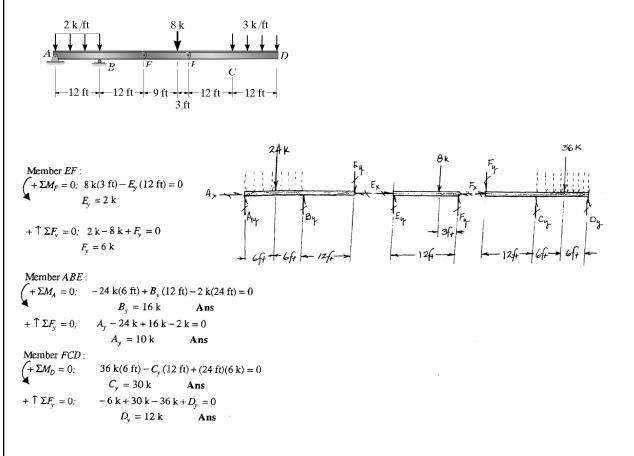


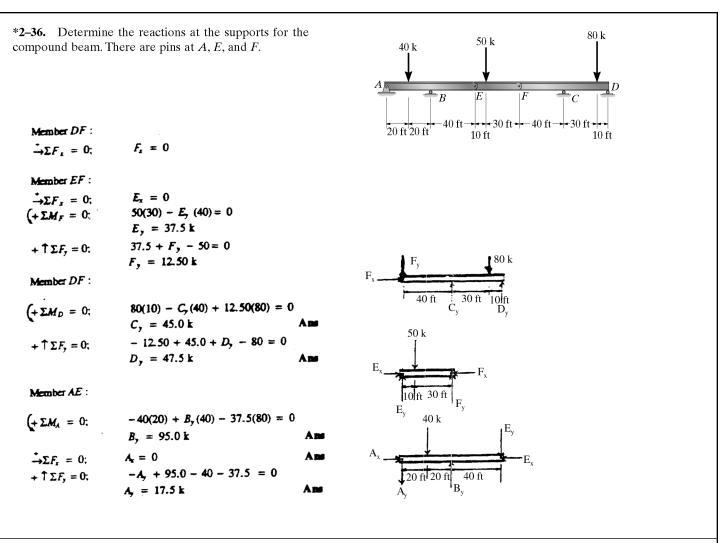




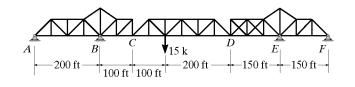
From $FBD$ (a)		
$+\Sigma M_{A} = 0; B_{y}(6) - 36(6) - 1.00(9) = 0$	$B_y = 37.5 \text{ k}$	Ans.
$+\downarrow \Sigma F_y = 0; A_y - 37.5 + 36 + 1.00 = 0$	$A_{y} = 0.50 \text{ k}$	Ans.
$+ \rightarrow \Sigma F_x = 0; \qquad A_x = 0$		Ans.

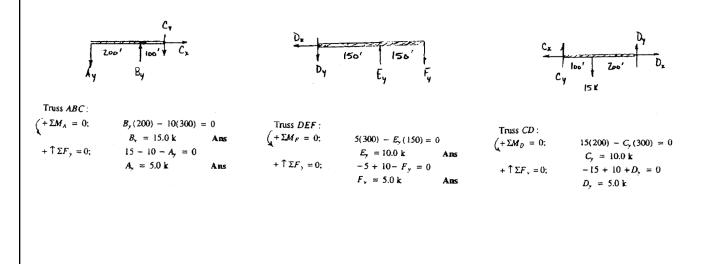
2-35. Determine the reactions at the supports A, B, C, and D.

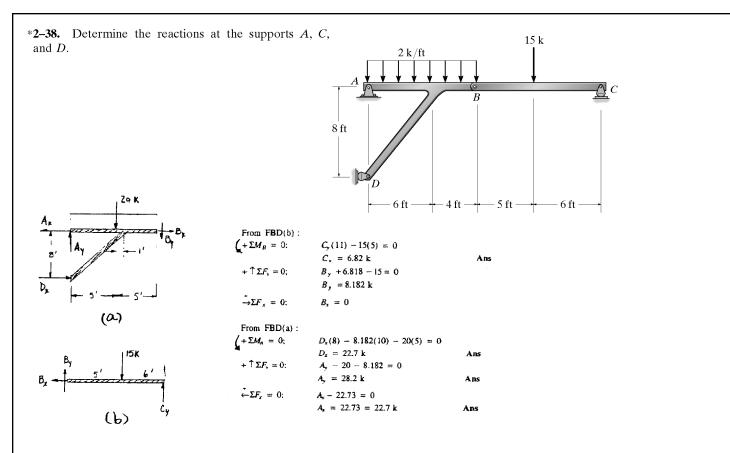




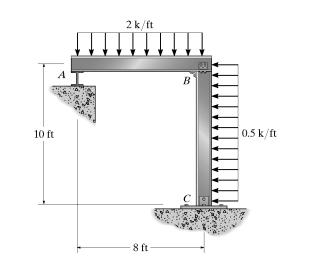
**2-37.** The construction features of a cantilever truss bridge are shown in the figure. Here it can be seen that the center truss CD is suspended by the cantilever arms ABC and DEF. C and D are pins. Determine the vertical reactions at the supports A, B, E, and F if a 15-k load is applied to the center truss.

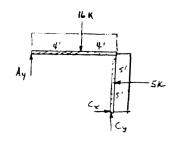




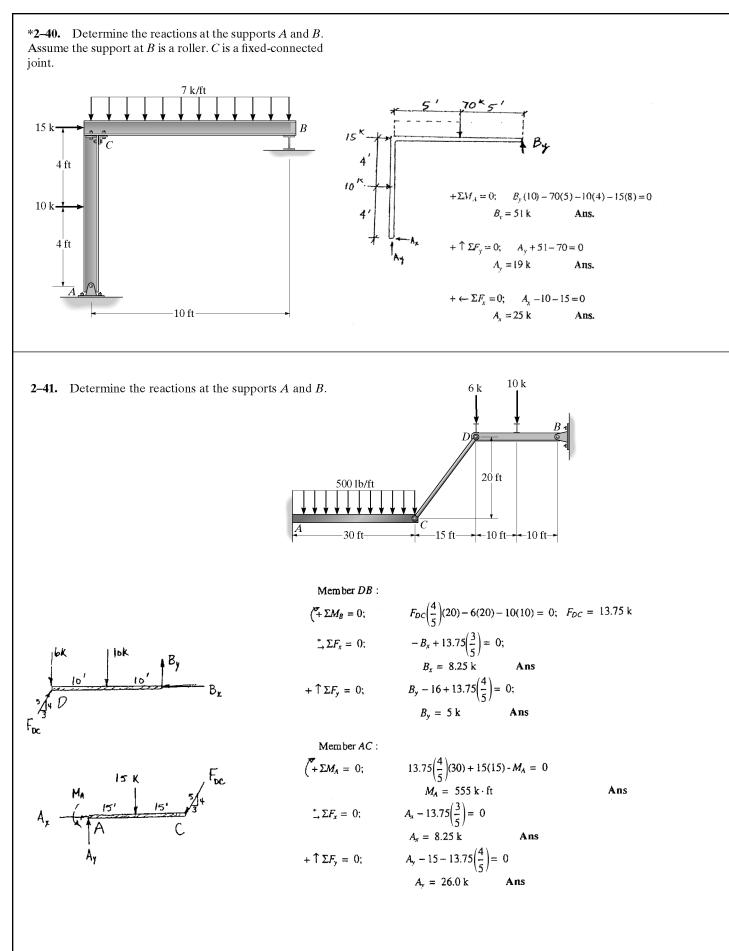


**2-39.** Determine the reactions at the supports A and C. Assume the support at A is a roller, B is a fixed-connected joint, and C is a pin.

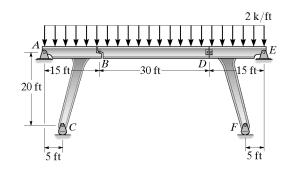




$(+\Sigma M_C = 0)$	$5(5) + 16(4) - A_1(8) = 0$	
<b>†•••</b>	$A_{y} = 11.125 = 11.1 \text{ k}$	Ans
$+\uparrow\Sigma F_{\star}=0;$	$11.125 - 16 + C_v = 0$	4
* === =	$C_{\rm v} = 4.875 = 4.88  \rm k$	Ans
$\rightarrow \Sigma F_x = 0$ :	$-5 + C_r = 0$ $C_r = 5.00 \text{ k}$	Ans
	$C_{\chi} = 0.00 \text{ k}$	AIS

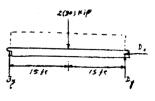


**2–42.** The bridge frame consists of three segments which can be considered pinned at A, D, and E, rocker supported at C and F, and roller supported at B. Determine the horizontal and vertical components of reaction at all these supports due to the loading shown.



## For segment BD :

$(+\Sigma M_D = 0;$	$2(30)(15) - B_{y}(30) = 0$	$B_y = 30$ kip	Ans
$\stackrel{+}{\rightarrow} \Sigma F_x = 0;$	$D_x = 0$		Ans
$+\uparrow\Sigma F_{2}=0;$	$D_{y} + 30 - 2(30) = 0$	$D_{\rm y}=30~{\rm kcip}$	Ans

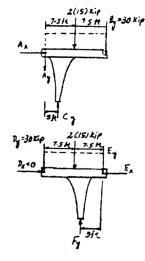


For segment ABC :

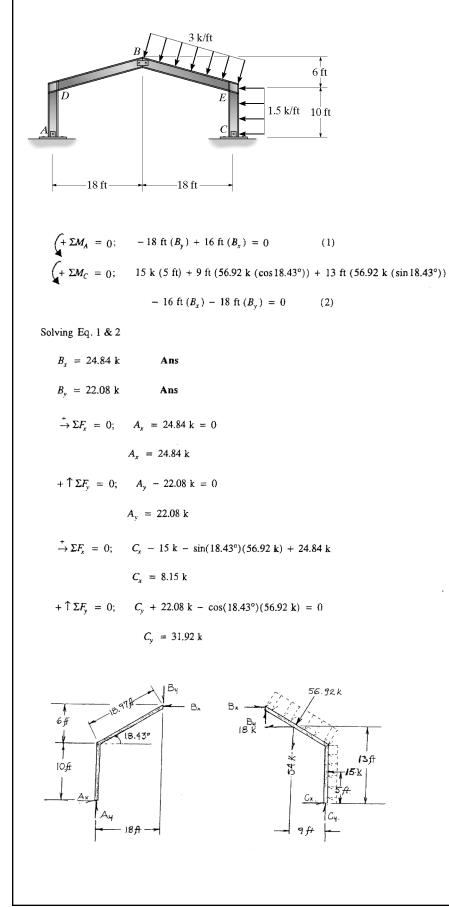
$\int +\Sigma M_A = 0;$	$C_{y}(5) - 2(15)(7.5) - 30(15) =$	$C_{y} = 135 \text{ kip}$	Ans
$\xrightarrow{*} \Sigma F_x = 0;$	$A_{\mathbf{x}} = 0$		Ans
$+\uparrow\Sigma F_{y}=0;$	$-A_{2} + 135 - 2(15) - 30 = 0$	A <sub>7</sub> = 75 kip	Ans

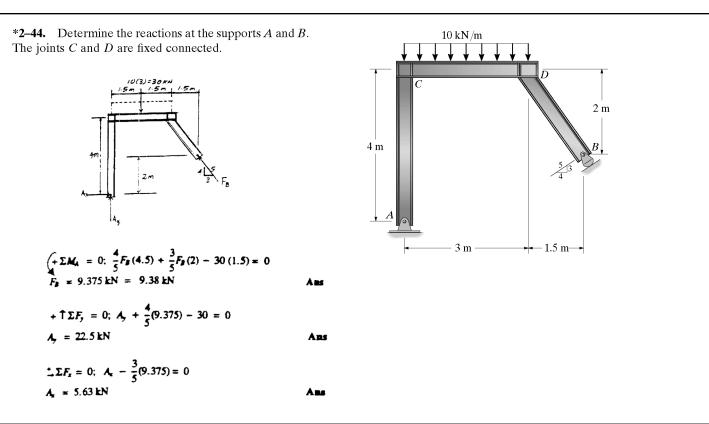
## For segment DEF :

$\int +\Sigma M_{\rm g} = 0;$	$-F_{r}(5) + 2(15)(7.5) + 30(15)$	= 0 F <sub>2</sub> = 135 kip	Ans
$\xrightarrow{+} \Sigma F_x = 0;$	$E_x = 0$		A me
$+\uparrow\Sigma F_{y}=0;$	$-E_{7}+135-2(15)-30=0$	$E_{\gamma} = 75  \mathrm{kip}$	Am



**2–43.** Determine the horizontal and vertical components at A, B, and C. Assume the frame is pin connected at these points. The joints at D and E are fixed connected.



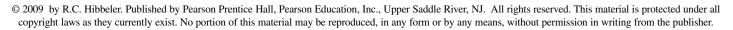


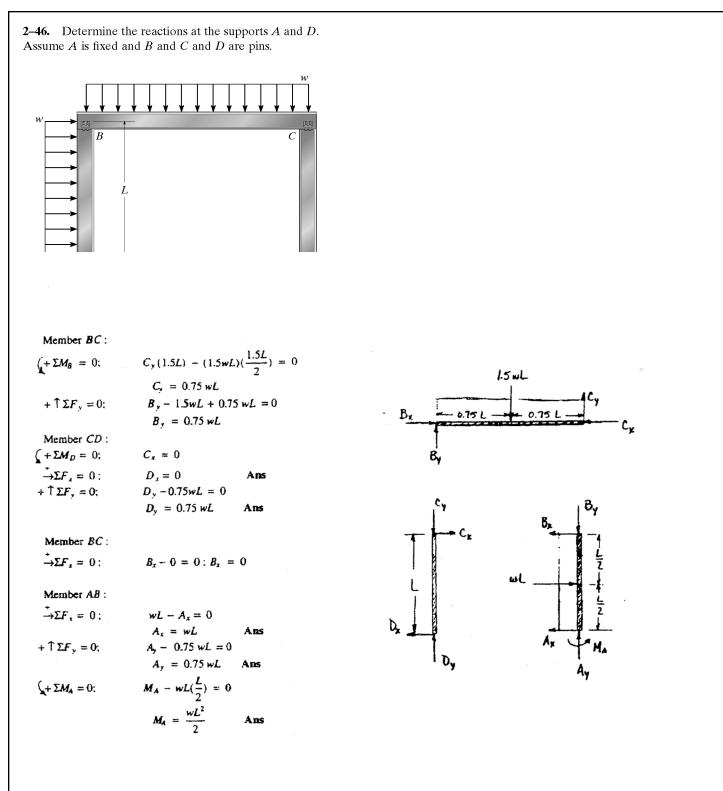
20 kN/m

© 2009 by R.C. Hibbeler. Published by Pearson Prentice Hall, Pearson Education, Inc., Upper Saddle River, NJ. All rights reserved. This material is protected under all copyright laws as they currently exist. No portion of this material may be reproduced, in any form or by any means, without permission in writing from the publisher.

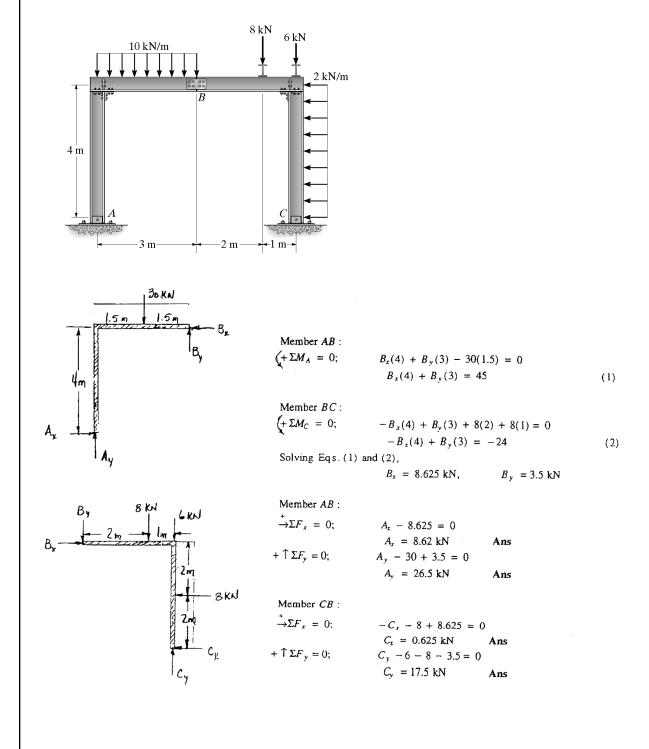
**2–45.** Determine the horizontal and vertical components of reaction at the supports *A* and *B*.

Member AD: DC  $(+\Sigma M_A = 0;$ 4 m  $-48 \text{ kN} (3 \text{ m}) + D_r (6 \text{ m}) = 0$  $D_x = 24 \text{ kN}$ 8 kN/m 6 m B $\stackrel{+}{\to} \Sigma F_x = 0;$  48 kN - 24 kN -  $A_x = 0$  $A_x = 24 \text{ kN}$ Member DCD: A  $\left(+\Sigma M_B = 0;\right)$ 5 m 100 kN (2.5 m) – 24 kN (4 m) +  $D_v$  (5 m) = 0  $D_{\rm v} = 30.8 \, \rm kN$ 100 KN  $+\uparrow \Sigma F_{y} = 0;$  30.8 kN - 100 kN +  $B_{y} = 0$  $B_y = 69.2 \text{ kN}$  $\stackrel{+}{\rightarrow} \Sigma F_x = 0; \qquad 24 \text{ kN} - B_x = 0$ Dy 6 m 2.5n  $B_x = 24 \text{ kN}$ 48 KN Member AD: 3m  $+\uparrow\Sigma F_y = 0;$  $-30.8 \text{ kN} + A_y = 0$ By 5m A.  $A_{v} = 30.8 \text{ kN}$ 

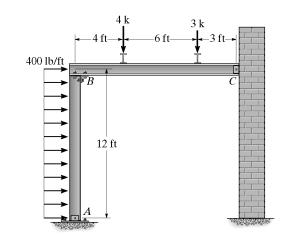




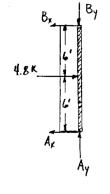
**2-47.** Determine the reactions at the supports A and C. The frame is pin connected at A, B, and C and the two joints are fixed connected.

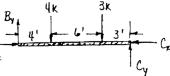


\*2-48. Determine the horizontal and vertical components of force at the connections A, B, and C. Assume each of these connections is a pin.

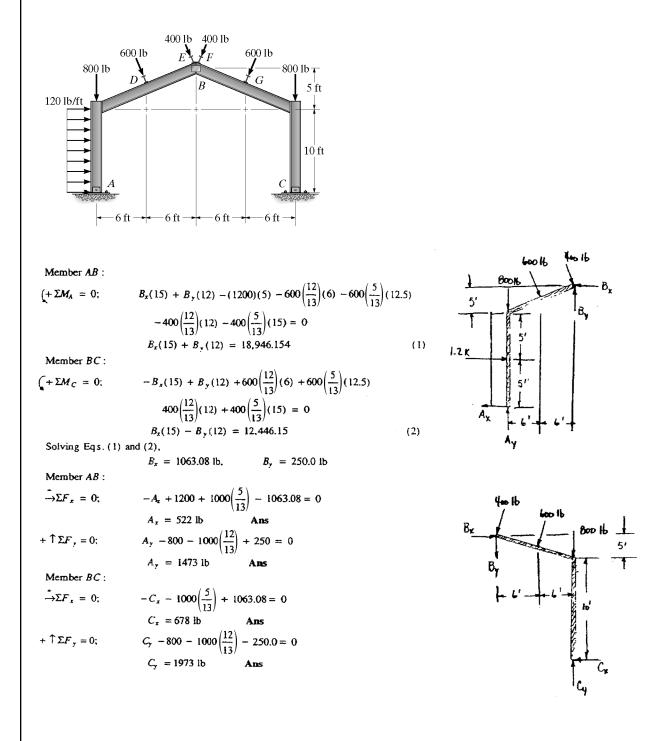


			Member AB :
	= 0	$B_x(12) - 4.8(6)$	$(+\Sigma M_A = 0;$
	Ans	$B_x = 2.40 \text{ k}$	<b>n</b>
4.	0	$A_x + 2.4 - 4.8 =$	$\stackrel{+}{\leftarrow} \Sigma F_x = 0;$
	Ans	$A_{\rm x} = 2.40 \ {\rm k}$	
	(1)	$A_{\rm y} - B_{\rm y} = 0$	$+\uparrow\Sigma F_y=0$ :
			Member BC:
	$\cdot 3(3) = 0$	$-B_y(13) + 4(9) +$	$(+\Sigma M_C = 0;)$
	Ans	$B_y = 3.46 \text{ k}$	*
	-3 = 0	$C_y + 3.462 - 4$	$+\uparrow\Sigma F_{y}=0;$
	Ans	$C_y = 3.54 \text{ k}$	
R		$C_r - 2.40 = 0$	$\stackrel{+}{\leftarrow} \Sigma F_x = 0;$
	Ans	$C_{\rm x} = 2.40 \ {\rm k}$	
P			From Eq. (1),
D <sub>x</sub>	Ans	$A_{\rm v} = 3.46 \ {\rm k}$	



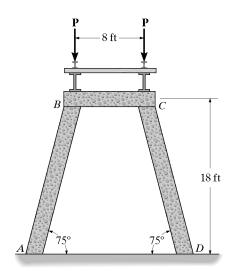


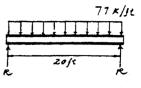
**2-49.** Determine the horizontal and vertical reactions at the connections A and C of the gable frame. Assume that A, B, and C are pin connections. The purlin loads such as D and E are applied perpendicular to the center line of each girder.



of reaction at the	e the horizontal and ve supports A, B, and C. at A, B, D, E, and F, a t C.	Assume the frame	8  kN/m $20  kN$ $12  kN$ $12  kN$ $F$ $3  m$ $C$ $3  m$ $C$
Member AD :			
$\langle +\Sigma M_A = 0;$	$-24(1.5) + D_x(3) = 0$ $D_x = 12 \text{ kN}$		מו
$\stackrel{+}{\rightarrow}\Sigma F_{x} = 0;$	$-12 + 24 - A_x = 0$		D <sub>1</sub> D <sub>y</sub>
	$A_x = 12 \text{ kN}$	Ans	โ เวิทนี
Member DE :			24 KN
$(+\Sigma M_E = 0:)$	$20(2) - D_y(4) = 0$		
-	$D_y = 10 \text{ kN}$		A <sub>x</sub>
$+\uparrow\Sigma F_{y}=0;$	$E_{y} - 20 + 10 = 0$ $E_{y} = 10 \text{ kN}$		ΥΥ.
$\stackrel{+}{\rightarrow}\Sigma F_{x} = 0;$	$-E_x + 12 = 0$		Zo KA
	$E_x = 12 \text{ kN}$		$4 D_y = 4 E_y$
Member AD :			$\Delta_{\mathbf{x}}$ $2m$ $2m$ $E_{\mathbf{x}}$
$+ \uparrow \Sigma F_{y} = 0;$	$A_{y} - 10 = 0$		
··· <b>_</b> , _,	$A_{\rm r} = 10  \rm kN$	Ans	
Member EF :	10(0) + F(4) = 0		
$(+\Sigma M_E = 0;$	$-12(2) + F_y(4) = 0$ $F_y = 6 \mathrm{kN}$		l freg
+ $\uparrow \Sigma F_{\gamma} = 0;$	$E_{y} - 12 + 6 = 0$		3m
	$E_{\rm r}=6{\rm kN}$		B.
Member BE :	n 10 6 - 0		'By
$+ \uparrow \Sigma F_{y} = 0;$	$B_y - 10 - 6 = 0$ $B_y = 16  kN$	Ans	
$(+\Sigma M_B = 0;$	$-12(3) + E_x(3) = 0$		
	$E_x = 12 \text{ kN}$		
$\rightarrow \Sigma F_x = 0;$	$-B_x + 12 - 12 = 0$		12 KN
	$B_{\star} = 0$	Ans	r' 1. 7. 1 7. 1 4
Member EF:			E E
$\stackrel{+}{\longrightarrow} \Sigma F_x = 0;$	$12 - F_x = 0;$		Ey
	$F_x = 12 \text{ kN}$		
Member FC:			
$\stackrel{+}{\rightarrow}\Sigma F_{r} = 0;$	$12 - C_x = 0;$		ι F <sub>i</sub>
	$C_x = 12 \text{ kN}$	Ans	F.
$+\uparrow\Sigma F_{y}=0;$	$C_{y}-6=0$		3.
, <u> </u>	$C_{\rm y} = 6  \rm kN$	Ans	
$(+\Sigma M_c = 0)$	$M_C - 12(3) = 0$		
$\sqrt{-2m_c} = 0$	$M_C = 36 \text{ kN} \cdot \text{m}$	Ans	
			i Cy

**2–1P.** The railroad trestle bridge shown in the photo is supported by reinforced concrete bents. Assume the two simply supported side girders, track bed, and two rails have a weight of 0.5 k/ft and the load imposed by a train is 7.2 k/ft (see Fig. 1–11). Each girder is 20 ft long. Apply the load over the entire bridge and determine the compressive force in the columns of each bent. For the analysis assume all joints are pin connected and neglect the weight of the bent. Are these realistic assumptions?



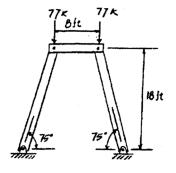


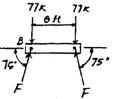
Maximum reactions occur when the live load is over entire span. Load = 7.2 + 0.5 = 7.7 k / ft R = 7.7(10) = 77 k

Then 
$$P = \frac{2(77)}{2} = 77 \text{ k}$$
  
All members are two-force members.  
 $\left(+\Sigma M_{\beta} = 0; -77(8) + F \sin 75^{\circ}(8) = 0\right)$ 

$$F = 79.7 \, k$$

Ans





Ans

It is not reasonable to assume the members are pin connected, since such a framework is unstable.